

ER 18/3/10 Planar core

Series/Type: B66480

Date: October 2022

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ER 18/3/10

Planar core B66480

Optimized winding area

■ Small overall footprint (core and winding)

■ Less EMI

Minimized winding length

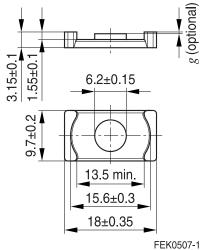
Delivery mode: single units

Magnetic characteristics (per set)

 Σ I/A = 0.732 mm⁻¹ I_e = 22.1 mm A_e = 30.2 mm²

 $A_{min} = 30.1 \text{ mm}^2$ $V_{P} = 667 \text{ mm}^3$

Approx. weight 3.5 g/set



1 LN0307-1

Ungapped

Material	A _L value nH	μ _e	P _V W/set	Ordering code
PC200	1200 ±25%	700	< 0.25 (50 mT, 1000 kHz, 100 °C) < 0.30 (30 mT, 2000 kHz, 100 °C)	B66480G0000X608
N49	1800 ±25%	1050	< 0.10 (50 mT, 500 kHz, 100 °C)	B66480G0000X149
N92	1800 ±25%	1050	< 0.39 (200 mT, 100 kHz, 100 °C)	B66480G0000X192
N87	2300 ±25%	1340	< 0.35 (200 mT, 100 kHz, 100 °C)	B66480G0000X187
N97	2300 ±25%	1340	< 0.30 (200 mT, 100 kHz, 100 °C)	B66480G0000X197

Other A_L values/air gaps and materials available on request – see Processing remarks on page 3.



Cautions and warnings

Mechanical stress and mounting

Ferrite cores have to meet mechanical requirements during assembling and for a growing number of applications. Since ferrites are ceramic materials one has to be aware of the special behavior under mechanical load.

As valid for any ceramic material, ferrite cores are brittle and sensitive to any shock, fast temperature changing or tensile load. Especially high cooling rates under ultrasonic cleaning and high static or cyclic loads can cause cracks or failure of the ferrite cores.

For detailed information see data book, chapter "General - Definitions, 8.1".

Effects of core combination on A₁ value

Stresses in the core affect not only the mechanical but also the magnetic properties. It is apparent that the initial permeability is dependent on the stress state of the core. The higher the stresses are in the core, the lower is the value for the initial permeability. Thus the embedding medium should have the greatest possible elasticity.

For detailed information see data book, chapter "General - Definitions, 8.1".

Heating up

Ferrites can run hot during operation at higher flux densities and higher frequencies.

NiZn-materials

The magnetic properties of NiZn-materials can change irreversible in high magnetic fields.

Ferrite Accessories

Our ferrite accessories have been designed and evaluated only in combination with our ferrite cores. We explicitly point out that our ferrite accessories or our ferrite cores may not be compatible with those of other manufacturers. Any such combination requires prior testing by the customer and will be at the customer's own risk.

We assume no warranty or reliability for the combination of our ferrite accessories with cores and other accessories from any other manufacturer.

Processing remarks

The start of the winding process should be soft. Else the flanges may be destroyed.

- Too strong winding forces may blast the flanges or squeeze the tube that the cores can not be mounted any more.
- Too long soldering time at high temperature (>300 °C) may effect coplanarity or pin arrangement.
- Not following the processing notes for soldering of the J-leg terminals may cause solderability problems at the transformer because of pollution with Sn oxyde of the tin bath or burned insulation of the wire. For detailed information see chapter "Processing notes", section 2.2.
- The dimensions of the hole arrangement have fixed values and should be understood as a recommendation for drilling the printed circuit board. For dimensioning the pins, the group of holes can only be seen under certain conditions, as they fit into the given hole arrangement. To avoid problems when mounting the transformer, the manufacturing tolerances for positioning the customers' drilling process must be considered by increasing the hole diameter.

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Cautions and warnings

Display of ordering codes for TDK Electronics products

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Symbols and terms

A Cross section of coil mm² $A_{e} = \text{Effective magnetic cross section} \\ A_{L} = \text{Inductance factor; } A_{L} = L/N^{2} \\ \text{nH} \\ A_{L1} = \text{Minimum inductance at defined high saturation } (\triangleq \mu_{a}) \\ \text{nH} \\ A_{min} = \text{Minimum core cross section} \\ A_{N} = \text{Minimum core cross section} \\ A_{R} = \text{Resistance factor; } A_{R} = R_{Cu}/N^{2} \\ \text{B} = \text{RMS value of magnetic flux density} \\ A_{B} = \text{Flux density deviation} \\ \text{B} = \text{Peak value of magnetic flux density} \\ \text{Vs/m², rowal} \\ \text{MB} = \text{Peak value of magnetic flux density} \\ \text{Vs/m², rowal} \\ \text{MB} = \text{Peak value of flux density} \\ \text{Vs/m², rowal} \\ \text{MB} = \text{Peak value of flux density} \\ \text{Vs/m², rowal} \\ \text{Vs/m², rowal} \\ \text{Vs/m², rowal} \\ \text{Vs/m², rowal} \\ \text{MB} = \text{Peak value of flux density} \\ \text{Vs/m², rowal} \\ Vs$	
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f _{Cu} Copper filling factor g Air gap mm	
g Air gap mm	
H RMS value of magnetic field strength A/m	
Ĥ Peak value of magnetic field strength A/m	
H _{DC} DC field strength A/m	
H _c Coercive field strength A/m	
h Hysteresis coefficient of material 10 ⁻⁶ cm/	4
h/μ_i^2 Relative hysteresis coefficient 10^{-6} cm/	4
I RMS value of current A	
I _{DC} Direct current A	
Î Peak value of current A	
J Polarization Vs/m ²	
k Boltzmann constant J/K	
k ₃ Third harmonic distortion	
k _{3c} Circuit third harmonic distortion	
L Inductance H = Vs/A	



Symbols and terms

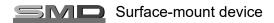
Symbol	Meaning	Unit
ΔL/L	Relative inductance change	Н
L ₀	Inductance of coil without core	Н
L _H	Main inductance	Н
L _p	Parallel inductance	Н
L _{rev}	Reversible inductance	Н
L _s	Series inductance	Н
l _e	Effective magnetic path length	mm
I _N	Average length of turn	mm
N	Number of turns	
P_{Cu}	Copper (winding) losses	W
P _{trans}	Transferrable power	W
P_V	Relative core losses	mW/g
PF	Performance factor	
Q	Quality factor (Q = ω L/R _s = 1/tan δ _L)	
R	Resistance	Ω
R _{Cu}	Copper (winding) resistance (f = 0)	Ω
R _h	Hysteresis loss resistance of a core	Ω
ΔR _h	R _h change	Ω
R _i	Internal resistance	Ω
R_p	Parallel loss resistance of a core	Ω
R _s	Series loss resistance of a core	Ω
R _{th}	Thermal resistance	K/W
R _V	Effective loss resistance of a core	Ω
s	Total air gap	mm
Т	Temperature	°C
ΔT	Temperature difference	K
T_{C}	Curie temperature	°C
t	Time	s
t _v	Pulse duty factor	
tan δ	Loss factor	
tan δ_l	Loss factor of coil	
tan δ_r	(Residual) loss factor at $H \rightarrow 0$	
tan $\delta_{\mathbf{e}}^{'}$	Relative loss factor	
tan δ_h	Hysteresis loss factor	
tan δ/μ _i	Relative loss factor of material at H \rightarrow 0	
U	RMS value of voltage	V
Û	Peak value of voltage	V
V _e	Effective magnetic volume	mm ³
Z	Complex impedance	Ω
Z _n	Normalized impedance $ Z _n = Z /N^2 \times \varepsilon (I_e/A_e)$	Ω/mm



Symbols and terms

Symbol	Meaning	Unit	
α	Temperature coefficient (TK)		
α_{F}	Relative temperature coefficient of material		
α_{e}	Temperature coefficient of effective permeability		
r	Relative permittivity		
Þ	Magnetic flux		
1	Efficiency of a transformer		
Ів	Hysteresis material constant		
li	Hysteresis core constant		
'S	Magnetostriction at saturation magnetization		
,	Relative complex permeability		
0	Magnetic field constant	Vs/Am	
а	Relative amplitude permeability		
арр	Relative apparent permeability		
е	Relative effective permeability		
i	Relative initial permeability		
p '	Relative real (inductive) component of $\overline{\mu}$ (for parallel components)		
p"	Relative imaginary (loss) component of $\overline{\mu}$ (for parallel components)		
r	Relative permeability		
rev	Relative reversible permeability		
s'	Relative real (inductive) component of $\overline{\mu}$ (for series components)		
s"	Relative imaginary (loss) component of $\overline{\mu}$ (for series components)		
tot	Relative total permeability		
	derived from the static magnetization curve		
	Resistivity	Ω m $^{-1}$	
I/A	Magnetic form factor	mm ⁻¹	
Cu	DC time constant $\tau_{Cu} = L/R_{Cu} = A_L/A_R$	s	
)	Angular frequency; ω = 2 Π f	s ⁻¹	

All dimensions are given in mm.





Important notes

The following applies to all products named in this publication:

- 1. Some parts of this publication contain statements about the suitability of our products for certain areas of application. These statements are based on our knowledge of typical requirements that are often placed on our products in the areas of application concerned. We nevertheless expressly point out that such statements cannot be regarded as binding statements about the suitability of our products for a particular customer application. As a rule, we are either unfamiliar with individual customer applications or less familiar with them than the customers themselves. For these reasons, it is always ultimately incumbent on the customer to check and decide whether a product with the properties described in the product specification is suitable for use in a particular customer application.
- 2. We also point out that in individual cases, a malfunction of electronic components or failure before the end of their usual service life cannot be completely ruled out in the current state of the art, even if they are operated as specified. In customer applications requiring a very high level of operational safety and especially in customer applications in which the malfunction or failure of an electronic component could endanger human life or health (e.g. in accident prevention or life-saving systems), it must therefore be ensured by means of suitable design of the customer application or other action taken by the customer (e.g. installation of protective circuitry or redundancy) that no injury or damage is sustained by third parties in the event of malfunction or failure of an electronic component.
- 3. The warnings, cautions and product-specific notes must be observed.
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